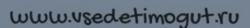


Анализ влияния положения сидя с дополнительной поддержкой спины в инвалидной коляске на распределение давления в ягодичной области

Автонотная некоттерческая организация «Все дети тогут»





Analysis of the influence of an articulated seat position for wheelchair on the pressure distribution in the gluteal region

Mariana Ribeiro Volpini Lana*, Paul Campos Santana Silva, Marcos Pinotti Barbosa

Abstract Introduction: The present study proposes a new scientific project for the seat of a wheelchair, suggesting that, through the properties of a three plan mobile seat, the pelvis of individuals with neuromotor dysfunctions may position themselves adequately, allowing a chain effect, with innumerable benefits to the users, such as prevention of deformities, of muscle shortening, of pressure ulcers and improved functionality. In spite of innumerable wheelchair models available in market, none presents the ample properties resembling the articulated seat, allowing the pelvic alignment that is crucial for the adoption of an adequate posture. **Methods**: The articulated seat was set over a ball and socket articulation made of two components, one convex that is fixed in the chair's structure and the other concave, attached to a mobile platform. The property of the articulated seat, to change the pressure distribution in the gluteal region, was tested on 34 typical individuals, without neurological injury, through a measurement system composed by 27 sensors. Results: The significance of the statistic model proposed determined that the articulated seat was capable of altering the pressure distribution in the gluteal region in several positions on the frontal and sagittal planes, in healthy subjects. Conclusion: Despite the fact that this equipment is capable of redistributing the pressure in a seating position, future research to examine other parameters such as time of use, the use in subjects with neurological dysfunction, the angle of pelvic inclination, the criterions of indication and non-indication, inter alia, must be conducted to appropriately qualify this device.

Keywords Bioengineering, Wheelchair, Pelvic alignment, Cerebral palsy.

Introduction

Cerebral Palsy (CP) is defined as "[...] a disorder of movement and posture due to a defect or lesion in the immature brain." (Bialik and Givon, 2009, p. 1). Children with cerebral palsy often use wheelchairs with special adaptations, aiming to improve posture and help prevent deformities. The Posture influences the cardiorespiratory function, the distribution of pressure points, the performance of the digestive tract, sleep and pain (Hägglund and Wagner, 2008; Vekerdy, 2007). In addition, a proper postural alignment could promote functionality and maximizes patient comfort (Hatta et al., 2007).

The position in which an individual is with a good body alignment is called neutral posture. In this posture an individual remains more relaxed since muscles do not need much effort to keep it. However, it is not an idle position, since in this state the person is ready to act (Zollars, 1996). The neutral posture is a reference for therapists who customize wheelchairs and it is expected that the individual in this posture is with the pelvis neutral (slightly forward) and weight on the ischial tuberosities, straight trunk, but with physiological curves preserved, hip and legs apart about 5-8° from the midline, knees and ankles joints

*e-mail: marivolpini@yahoo.com.br Received: 27 May 2013 / Accepted: 28 March 2014 with angles of 90° and feet resting on the support surface (Berger et al., 1990). Moreover, the head should be upright in the midline, allowing a view of the environment, shoulders relaxed and arms free to move and perform functions (Berger et al., 1990).

The position of the pelvis can tell us about the degree and the distribution of muscle tone of the individual (Holmes et al., 2003). Most spastic individuals (high tone) has a posterior pelvic tilt when seated normally, indicating an excessive activation of the hip extensor muscles, unlike a forward pelvic tilt usually indicates a very low tone (Holmes et al., 2003).

Observing a person with posterior pelvic tilt (Figure 1), for example, it's possible to realize the influence of the pelvis in the entire body positioning. The lower limbs tend to adduction and internal rotation with a concomitant knee extension and plantar flexion as an extensor pattern that started at the hip (Berger and Colangelo, 1982). This backward tilt of the pelvis also gives the individual a feeling of being "back" in space, unloading weight on the sacrum, and because of that this person tries to bring his body forward, tilting his torso with kyphosis, and hyper extending

the neck to compensate for the thoracic kyphosis (Berger and Colangelo, 1982).

Similarly, when the pelvis is tilted forward, righting reactions and equilibrium responses should result in extension of the head and trunk (back and torso head) and flexion of the hip and knee, as shown in Figure 2 (Cholewicki et al., 2000; Su-Fen et al., 2003).

The positioning of the pelvis affects the function of the trunk, head, neck, upper limbs and influences

the activation of muscle reflexes, since it provides a support base for the proximal segments of the body in the sitting posture (Batavia et al., 2001). Correcting pelvic alignment it's possible to alter the whole body positioning, resulting even in improvement of the hand function. Therefore it is essential that any evaluation in the sitting posture begins with the pelvis and that any intervention starts for its correction (Berger and Colangelo, 1982).



Figure 1. (a) Child with a backward pelvic tilt and (b) correction of the backward pelvic tilt with an anterior seat inclination (anterior wedge). Source: author's personal archive.

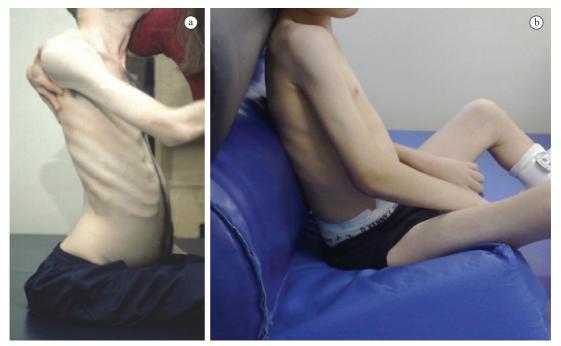


Figure 2. (a) Child with a forward pelvic tilt and (b) child with appropriate pelvic position after placing a posterior wedge. Source: 2° Brazilian Symposium of Seating (Simpósio..., 2008) and author's personal archive.

Several researches continue to investigate the positive and negative aspects of the custom adaptations by the wheelchair seating services and of the commercial models of wheelchair available on the market to assist the positioning of wheelchair users. In addition, new models are often proposed, but these have not emphasized the pelvic positioning, so they became ineffective or palliative. Since the pelvic alignment is crucial for the adoption of a proper sitting posture (Van Geffen, 2008a, 2008b), more cautious and creative seats projects, as well as pelvic support components are needed in order to obtain an optimized pelvic positioning.

Seeking to contribute to scientific and technological advancement in this area, this study aimed to propose a specific new design for wheelchair seat able to promote a better pelvic alignment and consequently adequate pressure distribution in sitting posture and to test it from its ability to redistribute the pressure in the gluteal region by varying its position.

Methods

This study developed the articulated wheelchair seat and tested its ability to alter the pressure distribution in the gluteal region, by changing its position in the frontal and sagittal planes, and using intensity maps as a resource for analysis. All the measuring system used to observe the distribution of pressure in the gluteal region in sitting posture consists of the articulated seat, 27 FSR sensors (Force Sensing Resistor) arranged along the surface of the seat (340×340 mm) and the data acquisition system associated with the software for processing and displaying the results.

The articulated seat

The seat was mounted on a ball and socket articulation. This joint is composed of two components, one convex and the other concave. The concave portion is fixed to the mobile platform where FSR sensors are arranged and the convex part is fixed to the frame of the wheelchair. This device installed centrally allows movement on the three planes (frontal, sagittal, transversal) independently or combined (precession).

The design includes the placement of adjustable mechanical limiters responsible for defining the maximum range of movement on the sagittal and frontal planes independently, as well as to control the rotation and the multi axial movement, therefore making the movement compatible to that which is desired. There are also springs around each backstop ensuring that the movements of the seat will be smooth. The articulated seat for wheelchair has a patent required under registration number PI- 0504703-0 (Volpini et al., 2007).

The mechanical part of the system can be better understood by means of the drawing of Figure 3, basically composed of ten components: 1) Ball and socket articulation; 2) Flange of the concave part (2.1)and of the convex part (2.2) of the ball and socket articulation; 3) Platform that supports the plywood with the FSR sensors, where is fixed the concave part of the Ball and socket articulation; 4) Hollow screw which regulates the preload of the spring; 5) Spring: for this study, specifically, springs were not used, since the positions evaluated were only static postures of individuals, but the calculations and the dimensions of them were determined; 6) Spring support "Cup" (external diameter: 34 mm, internal diameter: 26 mm, height: 50 mm); 7) Seat of plywood with 10 mm thick; 8) Screw that regulates the mechanical limiters; 9) Mounting of the spring box with the screw that adjusts the spring pre-tension and with the other screw that regulates the mechanical limiter; 10) FSR sensors.

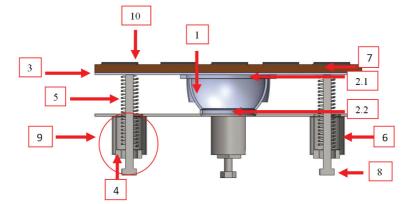


Figure 3. Articulated seat in cross-section. (1) Ball and socket articulation, (2.1) fastening flange of concave portion, (2.2) fastening flange of convex portion, (3) platform that supports the plywood, (4) screw that adjusts the preload spring, (5) spring, (6) spring support device, (7) wooden seat, (8) screw that regulates de mechanical limiter, (9) spring-screw device assembly, (10) FSR sensors.

Data acquisition system and capture software

The data acquisition system reads electric tension that comes from the Force Sensing Resistor (FSR) and converts these signals in equivalents values of force. Force Sensing Resistor (FSR) is a compact device, that shows a decrease in electrical resistance with an increase in the applied force on its surface (resistance is inversely proportional to the strength). In total, 27 FSR sensors were distributed over the surface of the seat (340×340 mm).

To view the results by LabView® software, intensity and surface curves with interpolation routines were used.

The calibration of the measurement system, to verify the behavior of the sensors under pressure, was according to NBR 8197:2002, items 7 and 8 of the Brazilian Association of Technical Standards – ABNT (Associação..., 2002), with the support of the Department of Physical tests of the Technological Center Foundation of Minas Gerais – CETEC/MG. All sensors of the measuring system are from brand Interlink Electronics, FSR408 model, with a nominal range of 10 kgf (5 mV). The results obtained during the calibration procedure were analyzed using the technique of regression and the coefficient of determination (R²) was the parameter considered to verify the accuracy of the technique.

The Intraclass Correlation Coefficient (ICC) was calculated for each sensor in order to determine their reliability. In sequence it was applied an Exploratory

Factor Analysis (EFA) to identify which sensors are grouped into variable groups (Factors) in order to facilitate the interpretation of the results. To ensure independence of observations, the values of each measurement were centralized as if in a panel model of random effects (random effects model), analyzing the deviations from the mean of each participant of the study, and not their original values. The Statistical Package for Social Science for Windows (SPSS) calculates an anti-image matrix of covariance and correlation. All diagonal elements of this matrix must be greater than 0.5, if the sample is adequate (Campos, 2000). Based on these conditions a solution with five Factors described in Figure 4 was obtained. The results show a good correlation between the Factors and the variables selected.

It is shown that the way in which the sensors are positioned tends to produce consistent results which generate the configuration obtained by EFA. The EFA also has good application conditions with Kaiser-Meyer-Olkin Measure of Sampling (KMO) which value is 0.872, close to the value of 0.900 that is excellent, showing that the sample is large enough to produce reliable results. Those sensors that not grouped generated Factor 6 and the sensor 18 was excluded from the analysis because it did not cluster with any of the others. Based on the results of the EFA an average of the pressures measured in each one of the six Factors described previously was calculated.

To check for differences between the measured mass in each one of the six Factors of the chair, for

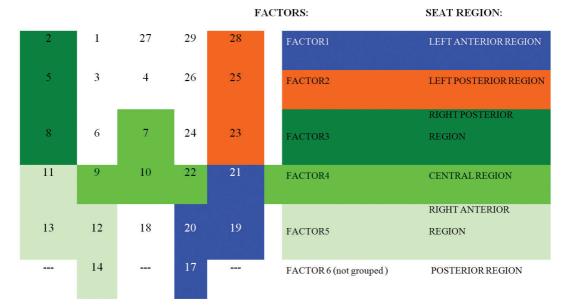


Figure 4. Schematic drawing of the top view of the seat with representation of Factors (found by grouping the sensors through Exploratory Factorial Analysis) by colors and of sensors by numbers.

each one of the five positions set in the study was employed Repeated Measures ANOVA.

Clinic methodology

The study involved the participation of 34 typical adults individuals, in other words, without neuromotor dysfunction, aged 20 to 50 years, female and male, with mass between 50 and 70 Kg. This population was selected randomly, for convenience, through the dissemination of the research in classrooms in the Department of Physiotherapy, Occupational Therapy and Physical Education, of the Federal University of Minas Gerais. The mixed sample (men and women) was chosen since, in both genders, proper sitting position (neutral position) is the same, defined as the situation in which the body weight is transferred to the chair seat by ischial tuberosity and soft tissue of the gluteal region, as well as to the ground through the feet. In this posture, compensatory movements are prevented, the loads are properly distributed and energy is conserved (Marques et al., 2010).

The participation of subjects aimed to assess the ability of the new articulated seat to redistribute pressure on the gluteal region, when adjusted properly seated posture.

The exclusion criteria were:

- Individuals with neuromotor dysfunction (neurological damage) or spinal curvatures deviations (scoliosis, kyphosis, lordosis) that could change the measurement results;
- Individuals outside the mass range between 50 kg to 70 kg.

Participants were evaluated by static postural inspection, in all three planes, to verify the absence of the spinal curvatures deviations.

This study was approved by the Research Ethics Committee Ethics of the Federal University of Minas Gerais (UFMG-COEP No 383/09) and Voluntary Informed Consent was signed by each participant, according to Resolution No. 196/96 of the Health National Council.

Evaluation measures and procedure

A protocol was established to ensure the standardization of research. It was requested that participants sit with their hands on the thighs, with horizontal gaze. The footrest was adjusted so that the angles between the torso and thigh and between the thigh and leg were equal to 90°. The data collection consisted of data acquisition of the pressure distribution in the gluteal region of the participants in five different seat positions. Over the measurement system was located a foam of 340×340 mm, density D60 and 5 cm thick, in which participants sat down and this allowed the proper reading of the sensors.

Five measurements for each of the five positions (adjustment) of the seat were performed (Caling and Lee, 2001; Defloor and Grypdonck, 1999; Hobson, 1992). They are: 1) seat without inclination, 2) 15° tilted forward, 3) 15° tilted backward, 4) 15° to the right; 5) 15° to the left.

Above 15° of pelvis tilt, individuals with righting reactions, simultaneously start trunk flexion in an attempt to maintain balance against gravity due to changes in body orientation. Thus, it can be said that above 15° of pelvic tilt the movement is not only from the hip but also from the spine (Cholewicki et al., 2000). Therefore, the maximum angle of adjustment of the seat in all planes was defined by 15° to ensure that the alignment would be only pelvic, but keeping the trunk free to make equilibrium responses and the righting reactions necessary for postural maintenance. These positions of the seat can be seen in Figure 5. All the seat's angles were measured by an Angle meter, 3 $\frac{1}{2}$ inches, from Dasco Pro Inc. and by a wood level of 14 inches from Famastil with two calibrated bubbles.

According to Gutierrez et al. (2004), three seconds is the necessary time to occur an accommodation in seated posture. Each one of the five measures was collected after three seconds, because then the accommodation time would be respected.

Variations in the position of the seat aim to promote a better posture alignment and hence better pressure distribution, and greater functionality in neurological patient.

The differences in the pressure distribution in the gluteal region in five different seat positions were compared to the initial position, by analyzing the intensity maps generated as well as through data obtained by the sensors and sent to the analysis software.

Results

The sample size is equal to 34 and was set considering the Central Limit theorem, since this allowed that the average tended to a normal distribution (Hual et al., 2005). This sample received also a high power effect (for significant effects above 80% in the analysis of variance), which is considered good. However, for some seat positions the power was lower, suggesting that other studies have a larger sample.

Multivariate test

The first global result of this study was obtained through multivariate statistical test that showed that only two variables influence the value of the mass measured in the different Factors of the chair. These variables are: a) the position (P) of the seat (within-subject factor) and b) the mass of individuals (between-subjects factor).

Analyzing the between-subjects factor (WEIGHT) the Table 1 shows that there is 0% chance of the weight of an individual to not affect the results, which means, the measured value.

Observing the intra-subject factor (position - P), the multivariate test showed that each seat position tends to generate a mass concentration in different regions of the seat or in other words, in different Factors of the seat (p = 0.010).

It is possible to see in Table 1 that considering the within-subjects factor (position - P) there is only a 1% chance of finding equal weights in different seating positions (b < 0.010).

These results were obtained by analyzing and comparing the generated values for the average mass in five different seat positions, and are compiled in Table 2. The data in Table 2 demonstrate the existence of significant effect (b < 0.010) from the seat position

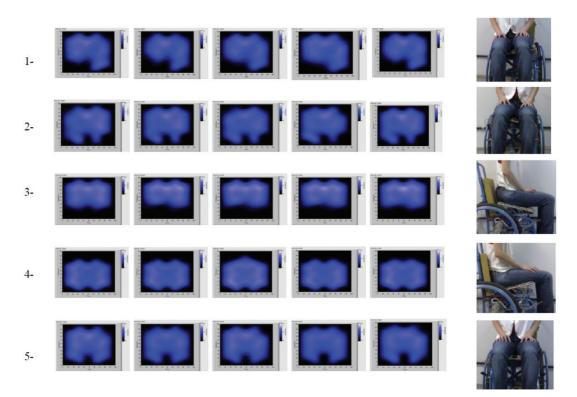


Figure 5. Five positions of the wheelchair articulated seat and the respective intensity maps acquired in the LabView software: 1 - five measurements with the seat tilted 15° to the right, 2 - five measurements with the seat tilted 15° to the left, 3 - five measurements with the seat tilted forward 15° , 4 - five measurements with the seat tilted back 15° , 5 - five measurements with flat seat, that means, without inclination.

 Table 1. Multivariate tests with the two variables capable of altering the measured values: 1) mass of participants (WEIGHT- between-subjects factor) and 2) sitting position (P- intra-subjects factor).

				Value	F	Std. Dev.	Sig
Between-subjects		Pillai's Trace	.720	11.576 ^b	6.000	27.000	.000*
	WEIGHT	Wilk's Lambda	.280	11.576 ^b	6.000	27.000	.000*
		Hotelling's Trace	2.573	11.576 ^b	6.000	27.000	.000*
		Roy's Largest Ro	2.573	11.576 ^b	6.000	27.000	.000*
Intra-subjects	Р	Pillai's Trace	.926	4.698 ^b	24.000	9.000	.010*
		Wilk's Lambda	.074	4.698 ^b	24.000	9.000	.010*
		Hotelling's Trace	12.527	4.698 ^b	24.000	9.000	.010*
		Roy's Largest Ro	12.527	4.698 ^b	24.000	9.000	.010*

WEIGHT- participants mass; P- position of the seat; F- F test; Std. Dev.- standard deviation; Sig-sig de b < 0.010; *Significant at 1% probability.

Intra-subjects effect		Value	F	Std. Dev.	Std.Erro	Sig
	Pillai's Trace	.281	1.584	24.000	504.000	.040*
WEIGHT	Wilk's Lambda	.739	1.622	24.000	430.000	.033*
	Hotelling's Trace	.326	1.653	24.000	486.000	.027*
	Roy's Largest Ro	.217	4.565 ^b	6.000	126.000	.000*
P*WEIGHT	Pillai's Trace	.319	1.819	24.000	504.000	.011*
	Wilk's Lambda	.711	1.844	24.000	430.306	.009*
	Hotelling's Trace	.367	1.856	24.000	486.000	.009*
	Roy's Largest Ro	.177	3.718 ^b	6.000	126.000	.002*

Table 2. Intra subjects effect comparing the average mass found in each of the five positions of the seat.

WEIGHT- average mass found in each one of the five seating positions; P*WEIGHT- combination of several mass of participants and seat position; F- F test; Std. Dev.- standard deviation; Std. Erro- erro do desvio padrão; Sig- sig de b < 0.010; *Significant at 1% probability.

(P-position), that means that the force that is applied in each region depends on both the tilt as the weight of the participant.

The multivariate test showed that the chance of finding a different pressure distribution pattern in the gluteal region in different seating positions was huge (94%). The analysis of univariate tests were conducted to verify where specifically these differences occurred, in other words, in which Factors of the chair (Table 3).

The results in Table 3 show, first, that there are differences between the values measured at each position of the wheelchair (b < 0.05), but it is also possible to observe that when this effect is combined with the weight of the patient, outcomes are altered (b < 0.05). These findings demonstrate that the study results should be adjusted by the weight of the participant to properly extract their conclusions. The Factors or the areas of the wheelchair seat where on which there was a significant effect can be seen in the schematic drawing of Figure 6, outlined in red.

Therefore, differences in the pattern of pressure distribution in the gluteal region occurred only in Factors 1, 2 and 5 (outlined in red). Considering the position (P) where, 1 – corresponds to 15° to the right, 2 – corresponds to 15° to the left, 3 – corresponds to 15° tilted forward, 4 – corresponds to 15° tilted backward and 5 – corresponds to the seat without inclination (flat) and the aforementioned Factors, it's possible to estimate the average mass of the Factors when the difference in weight of the study participants is controlled, in other words, with weights adjusted using the average weight, which corresponds to a value of mass 58 kg.

Delving some more into the results, since it was already known that the pressure was altered and in which Factors this change was significant, it was left to know in which seat positions this change was significant. This is interesting because one Factor considered insignificant to change the pressure in a specific position may have particular significance in

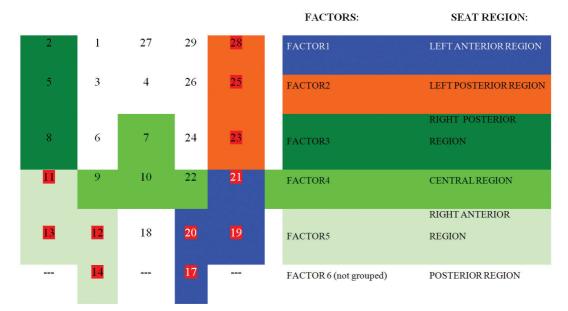


Figure 6. Factors with significant effect for changing the weight distribution in the five different positions.

Table 3. Evaluation of significant differences in the pressure distribution by means of univariate tests	Table 3. Evaluation of	significant differences	s in the pressure di	istribution by mean	s of univariate tests.
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Source	Mean		Sum of Squares type III	Std. Dev.	Average of Squares	F	Sig
		SphericityAssumed	192730.057	4	48182.514	3.034	.020
	F1	Greenhouse-Geisser	192730.057	2.953	65276.434	3.034	.034
	1.1	Huynh-Feldt	192730.057	3.387	56901.776	3.034	.027
		Lower-Bound	192730.057	1.000	192730.057	3.034	.091
		SphericityAssumed	337708.845	4	84427.211	2.360	.057
	F2	Greenhouse-Geisser	337708.845	2.447	138016.254	2.360	.090
	ΓZ	Huynh-Feldt	337708.845	2.747	122920.067	2.360	.082
		Lower-Bound	337708.845	1.000	337708.845	2.360	.134
		SphericityAssumed	224611.122	4	56152.780	1.282	.28
	F2	Greenhouse-Geisser	224611.122	1.923	116795.771	1.282	.28
	F3	Huynh-Feldt	224611.122	2.107	106579.237	1.282	.28
D		Lower-Bound	224611.122	1.000	224611.122	1.282	.26
Р		SphericityAssumed	8939.754	4	2234.938	.186	.94
		Greenhouse-Geisser	8939.754	2.568	3481.220	.186	.87
	F4	Huynh-Feldt	8939.754	2.899	3084.155	.186	.90
		Lower-Bound	8939.754	1.000	8939.754	.186	.66
		SphericityAssumed	181720.847	4	45430.212	3.822	.006
		Greenhouse-Geisser	181720.847	2.880	63090.970	3.822	.014
	F5	Huynh-Feldt	181720.847	3.294	55161.555	3.822	.010
		Lower-Bound	181720.847	1.000	181720.847	3.822	.059
		SphericityAssumed	100289.698	4	25072.424	.382	.82
		Greenhouse-Geisser	100289.698	1.225	79936.138	.382	.82
	F6	Huynh-Feldt	100289.698	1.322	75840.111	.382	.58
		Lower-Bound	100289.698	1.000	100289.698	.382	.59
		SphericityAssumed	225923.234	4	56480.808	3.556	.009
		Greenhouse-Geisser	225923.234	2.953	76518.750	3.556	.005
	F1	Huynh-Feldt	225923.234	3.387	66701.756	3.556	.013
		Lower-Bound	225923.234	1.000	225923.234	3.556	.012
	F2		400522.354	4	100130.588	2.799	.000
		SphericityAssumed Greenhouse-Geisser	400522.354	4 2.447		2.799	.025
		Huynh-Feldt	400522.354	2.447	163687.140 145783.077	2.799	.030
		Lower-Bound	400522.354	1.000	400522.354	2.799	.1045
		SphericityAssumed	217219.472	4	54304.868	1.240	.29
	F3	Greenhouse-Geisser	217219.472	1.923	112952.180	1.240	.29
		Huynh-Feldt	217219.472	2.107	103071.858	1.240	.29
* WEIGHT		Lower-Bound	217219.472	1.000	217219.472	1.240	.27
		SphericityAssumed	18410.422	4	4602.605	.384	.82
	F4	Greenhouse-Geisser	18410.422	2.568	7169.183	.384	.73
	- •	Huynh-Feldt	18410.422	2.899	6351.473	.384	.75
		Lower-Bound	18410.422	1.000	18410.422	.384	.54
		SphericityAssumed	180882.369	4	45220.592	3.804	.006
	F5	Greenhouse-Geisser	180882.369	2.880	62799.862	3.804	.014
	1.5	Huynh-Feldt	180882.369	3.294	54907.034	3.804	.010
		Lower-Bound	180882.369	1.000	180882.369	3.804	.060
		SphericityAssumed	10992.605	4	2748.151	.042	.99
	F4	Greenhouse-Geisser	10992.605	1.255	8761.682	.042	.88
	F6	Huynh-Feldt	10992.605	1.322	8312.722	.042	.89
		Lower-Bound	10992.605	1.000	10992.605	.042	.83

P- seat's position; P*WEIGHT- combination of several mass of participants and seat position; F1, 2, 3, 4, 5, 6- Factors of the seat; F- F test; Std. Dev.- standard deviation; Sig- sig de b < 0.05; *Significant at 5% probability.

another position P, in other words, the fact of not being significant to change the pressure in one position, does not determine that this Factor does not show significance for any of the five positions.

Then, to verify in which positions differences between the pressures occur, we applied the t-test with Bonferroni correction, comparing the differences of each Factor in the five positions, which allowed us to conclude that the change in seat position by tuning the wheelchair was able to redistribute the weight of the subjects in different areas of the seat, even when controlling the weight of these individuals.

Discussion

The results obtained in this study made it possible to analyze only the ability of the articulated seat designed to alter the pressure distribution in the gluteal region, by changing its position in the frontal and sagittal planes in healthy subjects. The likely benefits of this seat as well as the consequences of its use by wheelchair users have not been tested. New research to examine other parameters such as the time of use, the use by individuals with cerebral dysfunction, the angle of tilt of the pelvis, the indications and contraindications, among others, must be performed to properly qualify this device.

The sensors have been calibrated by the method of nonlinear regression using SPSS 15.0 statistic software for statistical data analysis. The nonlinear relationship was dealt as a multiple linear regression using exponential relationship. The estimation of nonlinear parameters was performed by the method of least squares, and the solution of the normal nonlinear equations was obtained by the Gauss-Newton process. The general form of the regression model is represented by Equation 1, where A, B, C, D are the estimated constants, for each sensor in a non-linear regression model, T is the voltage (V) and P is the pressure (N/ m²) concerning the sensors numerical readings.

$$T = A + [B\ln(P)] + [C(e)^{\frac{P}{D}}]$$
(1)

$Domain \in [0, 1Kg, 10Kg]$

Since we wish to express our results in Force, we will use Equation 2 to express the domain with this variable:

$$P = \frac{FORCE}{AREA} \tag{2}$$

It is important to note that the sensors area does not vary and it is equal to 1600 mm².

The model demonstrated good average value of the coefficient of determination (R^2), which was the considered parameter to check the accuracy of the regression technique. The adjustment values and the estimates of the constants of each one of the 32 sensors can be seen in Table 4. It's important to note that the electronic system consists of 27 sensors, but in total 32 sensors were calibrated in case there was a need to replace any of them. The data obtained by the calibration of the measurement system show that the lowest value found between the regression lines was 99.1% (Table 4).

Although these values have been quite satisfactory, the sensors 3, 4, 6, 22 and 24 showed low reliability, possibly due to the variable nature of the object of study, who are people, therefore, with varying responses. However, these sensors were not excluded, since in Exploratory Factor Analysis (EFA), which aimed to group them into Factors facilitating data analysis, they produced consistent results together, grouping properly.

It is interesting to note that the result of EFA generated a distribution of sensors in Factors, which coincides with the physical distribution of body segment analyzed through the measurement system, in other words, with the gluteus and thighs of the participants. It can be observed also that beyond this correlation exists another one related to the body symmetry in right and left sides. These results reinforce the coherence and efficiency of the EFA.

The reliability of the sensors, that is to say the ability of them to generate similar results verifying that the random and systematic errors are small, was tested by the Intraclass Correlation Coefficient (ICC). The interpretation of the values of the ICC can be understood as: $-0.4 \le \text{ICC} < 0.75$ represents a satisfactory reproducibility of the study; $-\text{ICC} < 0.4 \le \text{ICC} < 0.75$ says that the reproducibility of the study is excellent (Shrout and Fleiss, 1979) (Table 5).

Differences existed between the values measured at each position of the wheelchair seat, but this effect was only significant for the Factors F1, F2 and F5. It is interesting to note that two of the three Factors which were not significant have at least one sensor considered unreliable. For example, in Factor F3 all sensors have high reliability, however, the Factor F4 contains the sensor 22 with low reliability and the Factor F6 contains sensors 3, 4, 6 and 24 with low reliability, besides being the group of sensors that not answered satisfactorily in EFA. These sensors with low reliability can be one of the factors that have influenced the significance of their respective Factors.

It is noteworthy that the significance of only the Factors F1, F2 and F5 determine that the articulated seat is able to change the pressure distribution in different positions and situations, even when controlling the weight, so this equipment redistribute the pressure in the gluteal region.

When adjusting the seat, it was observed that each person has an own way of "correcting" the displacement of weight according to its own information from their several systems, and so compensating with different intensities of equilibrium responses of the trunk. It's possible to notice observing the intensity maps available in Figure 5, that pressure generally increased on the opposite side to the inclination, for example if the seat is tilted to the left, the highest intensity of weight discharge remained on the right side. This

Sensors	\mathbb{R}^2	Α	В	С	D
1	99.648	-419.80842	1006.88335	0.01531	-0.37078
2	99.092	-234.62126	810.89052	0.12132	-0.43440
3	99.807	-317.37842	847.86131	0.02882	-0.38530
4	99.517	-216.78756	777.51510	0.05983	-0.41750
5	99.854	-277.95085	863.41370	0.14357	-0.44537
6	99.620	-252.81377	875.04233	0.06228	-0.41211
7	99.647	-278.64272	942.64783	0.06223	-0.39443
8	99.741	-194.94944	790.61038	0.11119	-0.43606
9	99.838	-278.32981	828.45393	0.04712	-0.41253
10	99.799	-364.10874	1001.14370	0.03667	-0.39638
11	99.788	-340.77932	923.43759	0.02485	-0.38732
12	99.715	-259.10405	857.01790	0.07141	-0.42036
13	99.591	-288.22245	926.17148	0.05218	-0.40451
14	99.577	-345.93796	928.87352	0.02211	-0.37605
15	99.669	-435.14644	1035.66874	0.02631	-0.38424
16	99.769	-274.78276	934.03630	0.06328	-0.41579
17	99.791	-305.26184	914.20363	0.15487	-0.44885
18	99.556	-200.25184	807.75700	0.13483	-0.44541
19	99.545	-331.41653	1003.48773	0.01760	-0.37622
20	99.666	-300.50061	951.09945	0.05683	-0.41227
21	99.866	-236.77005	801.29274	0.12536	-0.44508
22	99.796	-234.46733	828.37284	0.13552	-0.44772
23	99.714	-305.61735	901.51087	0.10677	-0.43783
24	99.607	-286.26213	943.42974	0.06443	-0.41575
25	99.790	-179.72291	766.71992	0.09550	-0.42797
26	99.708	-84.84161	766.90931	0.12763	-0.44100
27	99.643	-269.15069	911.05249	0.03995	-0.40388
28	99.879	-195.50311	791.53660	0.11056	-0.43849
29	99.788	-147.28582	710.40838	0.18762	-0.46131
30	99.748	-282.93949	930.61279	0.03387	-0.39562
31	99.682	-229.85862	878.54553	0.14854	-0.44634
32	99.766	-331.31005	958.11385	0.02531	-0.38941

Table 4. Adjustment of the regression non linear model of the sensors calibration

R²- Coefficient of Determination; A, B, C, D- estimated constants for each sensor in a non-linear regression model.

probably occurred for two reasons: first because there was greater contact between the body segment and the higher side of the tilted seat, that is to say the right side, and second, because individuals corrected the weight shift using the trunk balance strategy which consists of tilt it to the right.

Taking the horizontal plane (seat without inclination – P-5) of Figure 5 as a reference for analyzing the pressure distributions in the other four seat positions, it is possible to make some interesting observations. First, it can be seen that the intensity maps of the position of the seat without inclination (P-5) are not fully symmetrical for the distribution of pressure. This is because no individual is symmetrical, with one side equal to the other, they are just similar (Buchanan and Horak, 2003; Lanzetta et al., 2004). Also analyzing the positions 1 - and 2 - of the Figure 5 it can be seen again that the compensation to the right

and left sides, resulting from the seat tilt 15° right and left, are different, demonstrating that the pattern of postural correction to one side is not equal to the other one in the same person.

It is interesting to correlate these observations with the Factors significance results. It has been observed in the results a lack of symmetry of them, since F2 (left posterior region) of Figure 5 showed significance to change the pressure distribution and your symmetrically opposite Factor, F3 (right posterior region) didn't show the same significance.

Considering the wheelchairs that are available and commonly found in the Brazilian market, we can appoint three models: Standard wheelchair with closure in X, recliner wheelchair, wheelchair with tilt in space. The wheelchair with closure in X is by far the most widely prescribed worldwide, due to the

Table 5. ICC of sensor's measurements, determining their reliability. $0.4 \le ICC \le 0.75$ – satisfactory reproducibility; ICC ≤ 0.4 – poor
reproducibility; ICC $\ge 0.75 - \text{excellent reproducibility}$.

Sensor	15°Right	15°Left	15°Forward	15°Backward	Flat	ICC of each sensor
1	0.94	0.98	0.69	0.90	0.55	0.81
2	0.97	0.92	0.77	0.90	0.90	0.89
3	0.45	0.57	-0.49	-0.33	-0.86	-0.13
4	0.18	0.95	0.38	-0.09	0.28	0.34
5	0.95	0.94	0.44	0.69	0.48	0.70
6	0.42	0.55	-0.70	0.04	0.21	0.10
7	0.79	0.95	0.96	0.32	0.72	0.75
8	0.93	0.87	0.92	0.40	0.98	0.82
9	0.85	0.97	0.98	0.23	0.80	0.77
10	0.98	0.95	0.98	0.95	0.98	0.97
11	0.93	0.97	0.96	0.58	0.93	0.88
12	0.96	0.99	0.95	0.46	0.96	0.86
13	0.98	0.99	0.74	0.98	0.98	0.93
14	0.98	0.99	0.80	0.95	0.96	0.94
15						
16						
17	0.93	0.94	0.96	0.32	0.97	0.83
18	0.98	0.96	0.83	0.97	0.77	0.90
19	0.97	0.97	0.72	0.36	0.98	0.80
20	0.98	0.94	0.97	0.10	0.81	0.76
21	0.94	0.96	0.98	0.95	0.92	0.95
22	0.23	0.58	0.98	0.96	-1.98	0.15
23	0.84	0.87	0.99	-0.07	0.96	0.72
24	0.58	0.20	0.49	0.06	0.20	0.30
25	0.97	0.83	0.51	0.95	0.33	0.72
26	0.73	0.52	0.97	0.90	0.37	0.70
27	0.87	0.70	0.33	0.95	0.20	0.61
28	0.90	0.96	0.81	0.79	0.91	0.87
29	0.97	0.92	0.73	0.97	0.88	0.89
30						
31	0.95	0.87	0.96	0.56	0.99	0.87
32						
ICC of each position	0.83	0.85	0.70	0.56	0.58	0.70
ICC (Exclusion)	0.93	0.91	0.82	0.66	0.80	0.82

simplicity of design and consequently low cost, without allowing positioning adjustments (Brubaker, 1986).

The recliner wheelchairs accept adjusts of the backrest angle that can be performed while the user is seated on the equipment, but without possibility to changing the positioning of the pelvis (Berger et al., 1990).

Wheelchairs with tilt in space allow to be angled backwards as a whole, while the sitting posture of wheelchair remains unchanged, since there isn't change in the angle between the backrest and seat, in other words not changing the position of the pelvis (MacDonald et al., 2009).

It was observed that, despite the numerous models of wheelchairs available, none of them have the extensive properties similar to the articulated seat, since the pelvic alignment is crucial to adopt a proper posture (Van Geffen, 2008b). The articulated seat was designed for patients with different types of neuromotor dysfunctions, who need help with body alignment for proper positioning, however emphasis was given to cerebral palsy due to their complexity of impairments.

The results obtained in this study enabled us to analyze only the ability of the articulated seat designed to alter the pressure distribution in the gluteal region, by changing your position in the frontal and sagittal planes in healthy subjects. The likely benefits of this seat as well as the consequences of its use by wheelchair users have not been tested. New research

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to analyze other parameters such as the time of use, the use by individuals with neuromotor dysfunction, the angle of tilt of the pelvis, the indications and contraindications, among others, must be performed to properly qualify this device.

Overall, this paper shows a new method for designing wheelchairs with articulated seats. The tests performed with 34 healthy participants, that is to say without neuromotor dysfunction, demonstrated that the articulated seat is able to redistribute the pressure in the gluteal region after his inclination in the frontal and sagittal planes, however, need for improvements were detected in the mechanical and electronic projects.

It can be said that the objectives of this research were achieved and among the goals that this mechanical design is proposed, not all were been evaluated yet, for example, the rotation and precession movements of the seat as well as its use by wheelchair users.

Other studies should be conducted in order to provide more support for a more careful analysis of the likely benefits of this equipment.

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References

Associação Brasileira de Normas Técnicas. ABNT/CB-04: Máquinas e Equipamentos Mecânicos – Materias metálicos – Calibração de instrumentos de medição de força de uso geral. Rio de Janeiro: ABNT; 2002.

Batavia M, Batavia AI, Friedman R. Changing chairs: anticipating problems in prescribing wheelchairs. Disability and Rehabilitation. 2001; 23(12):539-48. PMid:11432651. http://dx.doi.org/10.1080/09638280010022531

Berger A, Colangelo C. Positioning the client with C.N.S. deficits: the wheelchair & other adapted equipment. New York: Valhalla; 1982. p. 5-22.

Berger A, Presperin J, Tallman T. Positioning for function: wheelchairs and other assistive technologies. New York: Valhalla; 1990. p. 21-50.

Bialik GM, Givon U. Cerebral Palsy: classification and etiology. Acta Orthopaedica et Traumatologica Turcica. 2009; 43(2):77-80. PMid:19448345. http://dx.doi.org/10.3944/ AOTT.2009.077

Brubaker CE. Wheelchair prescription: an analysis of factors that affect mobility and performance. Journal of Rehabilitation Research and Development. 1986; 23(4):19-26. PMid:3820118.

Buchanan JJ, Horak FB. Voluntary control of postural equilibrium patterns. Behavioural Brain Research. 2003; 143:121-40. http://dx.doi.org/10.1016/S0166-4328(03)00038-X

Caling B, Lee M. Effect of direction of applied mobilization force on the postero-anterior response in the lumbar spine. Journal of Manipulative and Physiological Therapeutics. 2001; 24(2):71-8. PMid:11208218. http://dx.doi.org/10.1067/mmt.2001.112568

Campos D. Psicologia da adolescência. 17. ed. Petrópolis: Vozes; 2000. p. 157.

Cholewicki J, Polzhofer GK, Radebold A. Postural control of trunk during unstable sitting. Journal of Biomechanics. 2000; 33(12):1733-7. http://dx.doi.org/10.1016/S0021-9290(00)00126-3

Defloor T, Grypdonck MH. Sitting posture and prevention of pressure ulcers. Applied Nursing Research. 1999; 12(3):136-42. http://dx.doi.org/10.1016/S0897-1897(99)80045-7

Gutierrez EM, Alm M, Hulting C, Saraste H. Measuring seating pressure, area, and asymmetry in persons with spinal cord injury. Europe Spine Journal. 2004; 13:374-9. PMid:14639505 PMCid:PMC3468044. http://dx.doi. org/10.1007/s00586-003-0635-7

Hägglund G, Wagner P. Development of spasticity with age in a total population of children of cerebral palsy. BMC Musculoskeletal Disorders. 2008; 9:150. PMid:18990204 PMCid:PMC2644696. http://dx.doi.org/10.1186/1471-2474-9-150

Hatta, T, Nishimura S, Inoue K, Yamanaka M, Maki M, Kobayashi N, Kishigami H, Sato M. Evaluating the relationships between the postural adaptation of patients with profound cerebral palsy and the configuration of the seating Bugg's seating support surface. Journal of Physiological Anthropology. 2007; 26(2):217-24. PMid:17435368. http://dx.doi.org/10.2114/jpa2.26.217

Hobson DA. Comparative effects posture on pressure and shear the body seat interface. Journal of Rehabilitation Research & Development. 1992; 29(4):21-31. http://dx.doi. org/10.1682/JRRD.1992.10.0021

Holmes KJ, Michael SM, Thorpe SL, Solomonidis SE. Management of scoliosis with special seating for the nonambulant spastic cerebral palsy population-a biomechanical study. Clinical Biomechanics. 2003; 18:480-7. http://dx.doi. org/10.1016/S0268-0033(03)00075-5

Hual J, Xiong Z, Lowey J, Suh E, Dougherty E. Optimal number of features as a function of sample size for various classification rules. Bioinformatics. 2005; 21(8):1509-15. PMid:15572470. http://dx.doi.org/10.1093/bioinformatics/ bti171

Lanzetta D, Cattaneo D, Pellegatta D, Cardini R. Trunk control in unstable sitting posture during functional activities in healthy subjects and patients with multiple sclerosis. Archives of Physical Medicine and Rehabilitation. 2004; 85:279-83. PMid:14966714. http://dx.doi.org/10.1016/j. apmr.2003.05.004

MacDonald B, Kirby RL, MacLeod DA, Webber A. Sitting pressure in the tilted position. American Journal of Physical

Medicine & Rehabilitation. 2009; 88(1):61-5. PMid:18971771. http://dx.doi.org/10.1097/PHM.0b013e31818dff2a

Marques NR, Hallal CZ, Gonçalves M. Características biomecânicas, ergonômicas e clínicas da postura sentada: uma revisão. Fisioterapia e Pesquisa. 2010; 17(3):270-6. http://dx.doi.org/10.1590/S1809-29502010000300015

Simpósio Brasileiro de Adequação Postural em Cadeira de Rodas – Seating: Anais do II Simpósio Brasileiro de Adequação Postural em Cadeira de Rodas – Seating; 2008 ago, São Paulo. São Paulo; 2008.

Su-Fen L, Yang TF, Hsu TC, Chan RC, Ta-Sen W. Differences in seated postural control in children with spastic cerebral palsy and children who are typically developing. American Journal of Physical Medicine & Rehabilitation. 2003; 82(8):622-6. PMid:12872019. http://dx.doi.org/10.1097/01. PHM.0000073817.51377.51

Shrout PE, Fleiss JL. Intraclass correlation: uses in assessing rater reliability. Psychological Bulletin. 1979; 86(2):420-8. http://dx.doi.org/10.1037/0033-2909.86.2.420

Van Geffen P, Moller BI, Reenalda J, Veltink PH, Koopman BF. Body segments decoupling in sitting: control of body posture from automatic chair adjustments. Journal of Biomechanics. 2008a; 41:3419-25. PMid:18996530. http:// dx.doi.org/10.1016/j.jbiomech.2008.09.017

Van Geffen P, Reenalda J, Veltink PH, Koopman BF. Effects of sagital postural adjustments on seat reaction load. Journal of Biomechanics. 2008b; 41:2237-45. PMid:18533160. http://dx.doi.org/10.1016/j.jbiomech.2008.04.012

Vekerdy Z. Management of seating posture of children with cerebral palsy by using thoracic-lumbar-sacral orthosis with non-rigid SIDO frame. Disability and Rehabilitation. 2007; 29(18):1434-41. PMid:17729090. http://dx.doi. org/10.1080/09638280601055691

Volpini MR, Volpini E, Pinotti M, Silva P. Assento articulado nos três planos, permitindo movimento pélvico ânteroposterior, látero-lateral, de rotação e de precessão. Rio de Janeiro: INPI; 2007.

Zollars JA. Special seating: an illustrated guide. Minneapolis: Reha Otto Bock; 1996.

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